



Advances in SiC Power Technology

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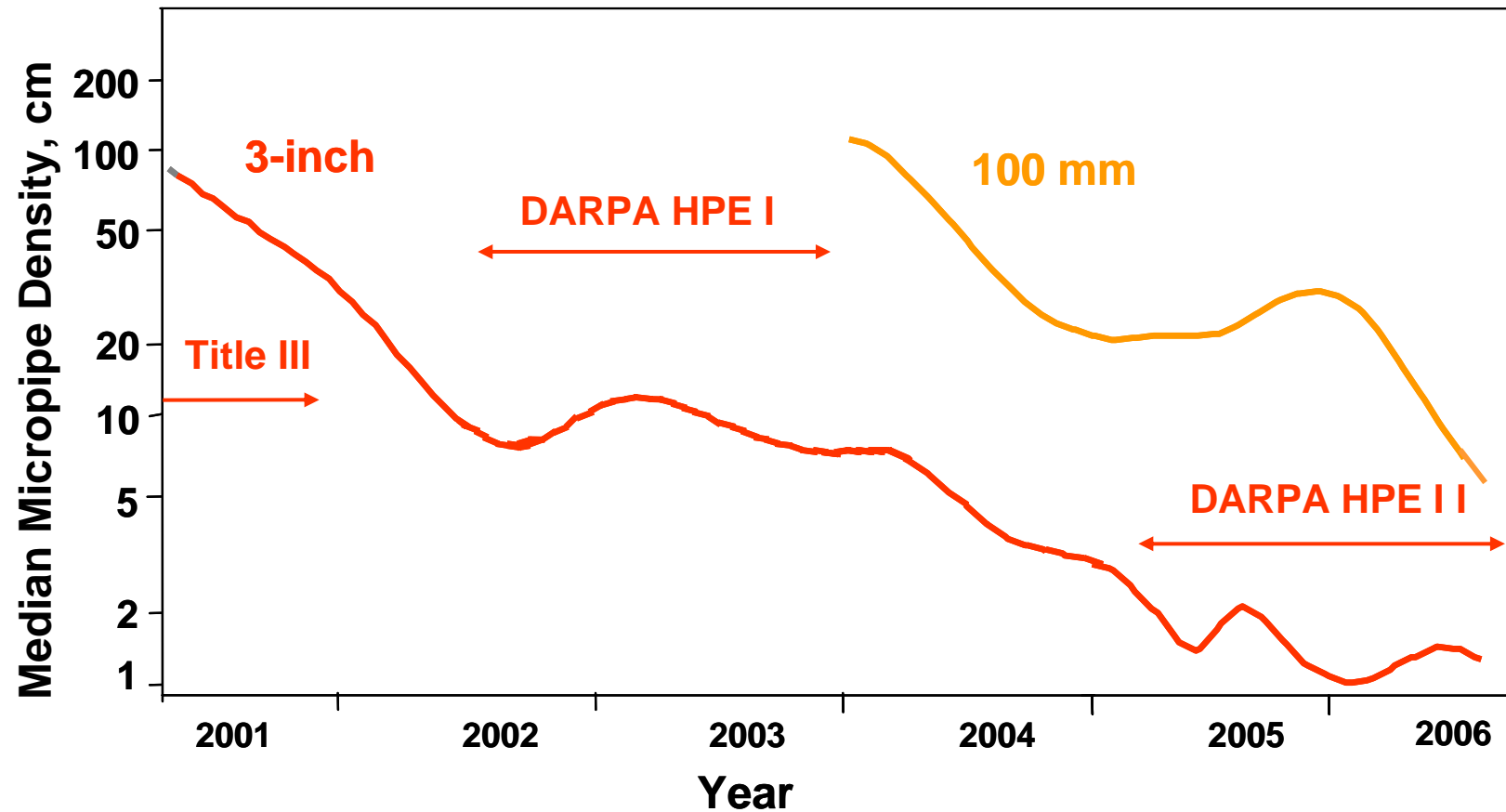
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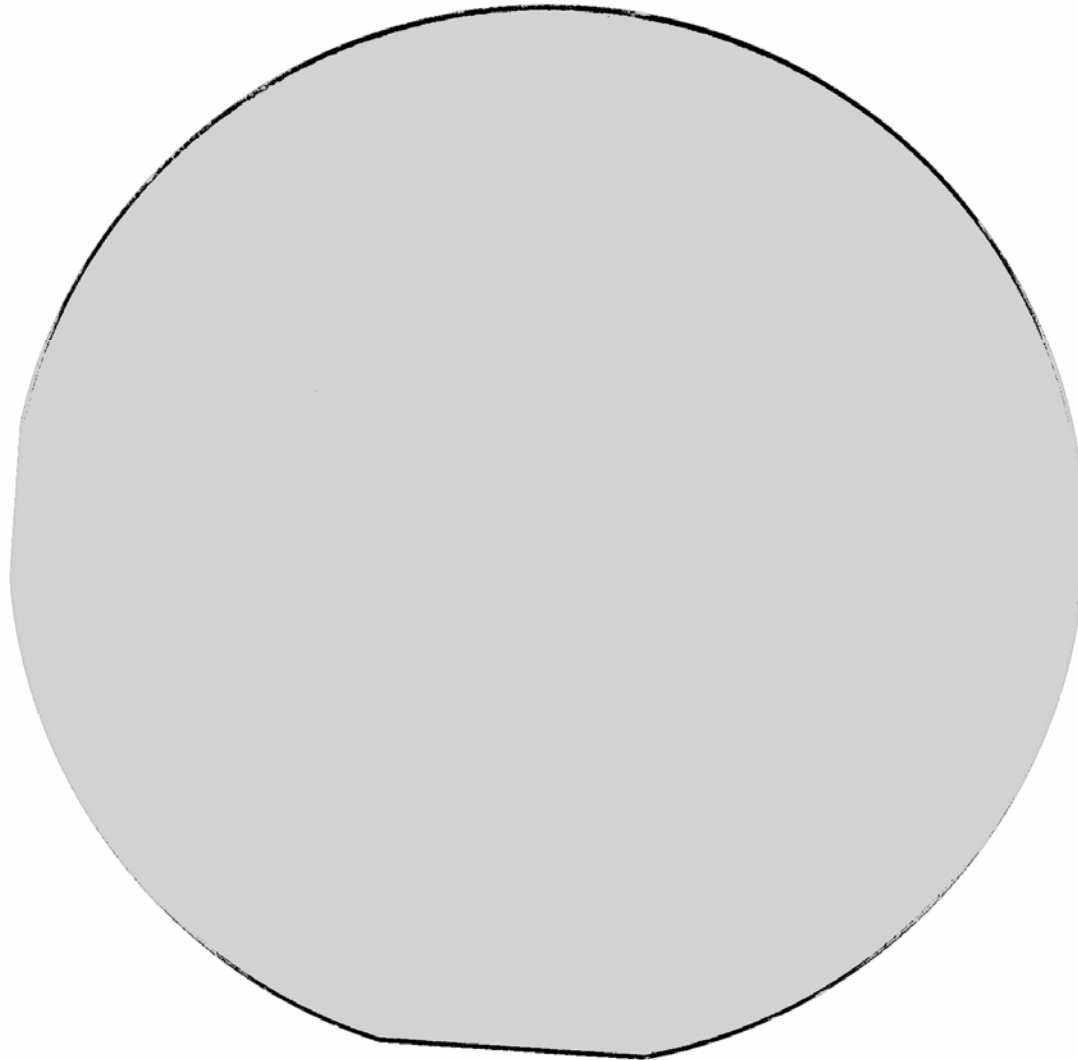
Monthly Median Production MPD



100-mm work supported by ARL MTO (W911NF-04-2-0021) and DARPA (N00014-02-C-0306)



3-inch 4HN SiC Wafer Production Process Quality

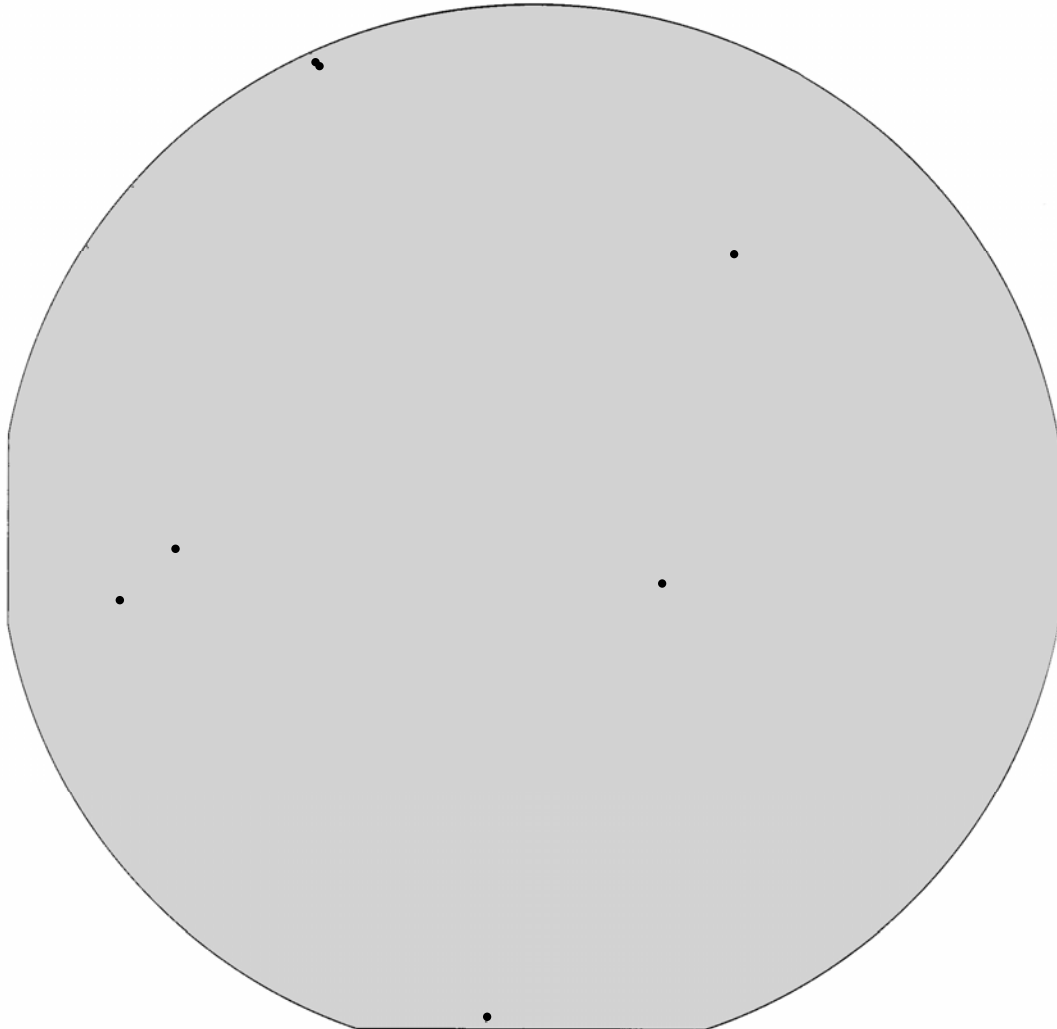


- **Best Production
3-inch 4HN SiC wafer
MPD = 0.02 cm^{-2}**
- **Best R&D 3-inch
4HN SiC Wafer
MPD = 0.00 cm^{-2}**

ZMP

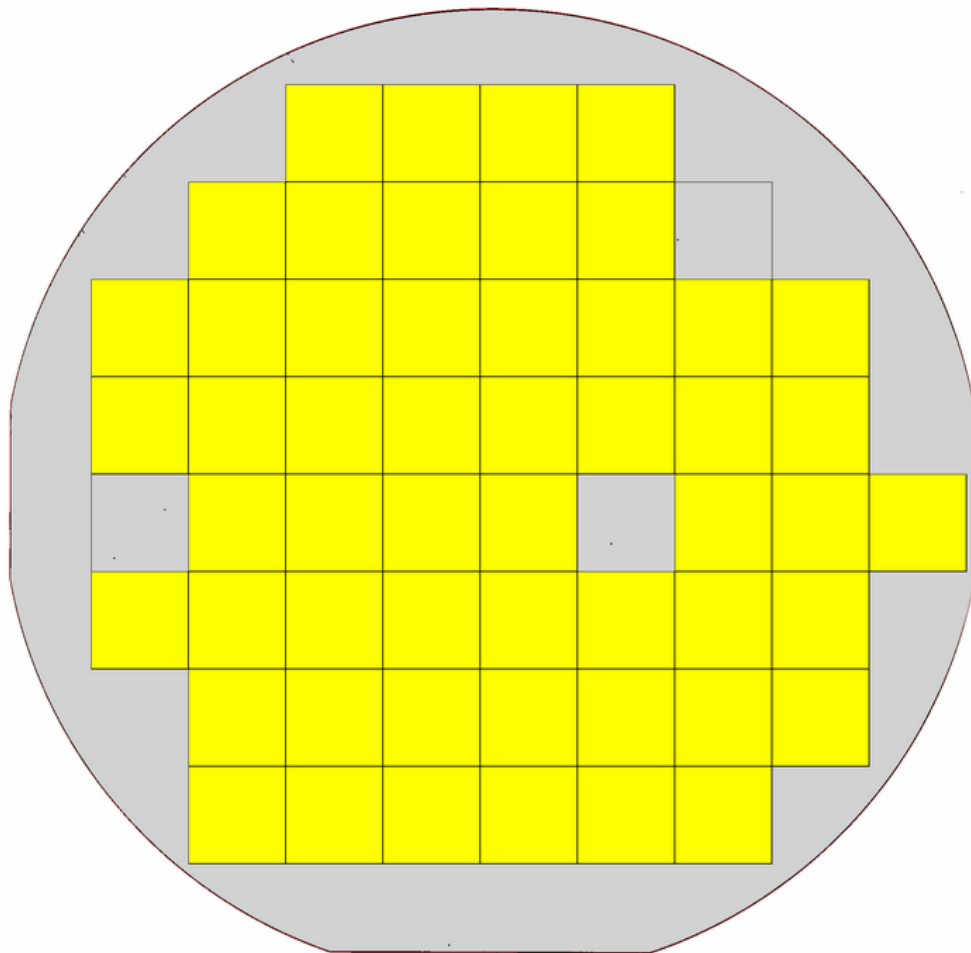


100 mm 4HN-SiC Wafer Production Process Quality



- **Almost Double the Area of a 3-inch 4HN-SiC Wafer**
- **Lowest MPD for 100 mm 4HN-SiC With MPD = 0.1 cm⁻²**
- **Median MPD < 5 cm⁻² in Production Process**

Projected Device Yield From Lowest MPD 100 mm Wafer Thus Far



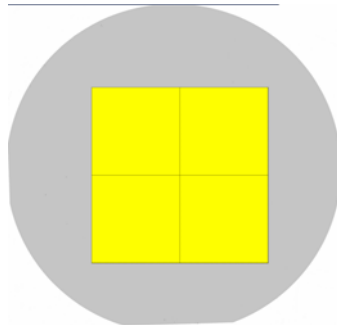
- Projected Yield for 1 cm² Devices
- Assume Device Failure Only From Micropipes

- Micropipe Density = 0.1 cm⁻²
- **Projected Device Yield > 94%**
- Yielded Devices = 53
- 65% More Devices Than Ideal 3-inch 4HN SiC Wafer

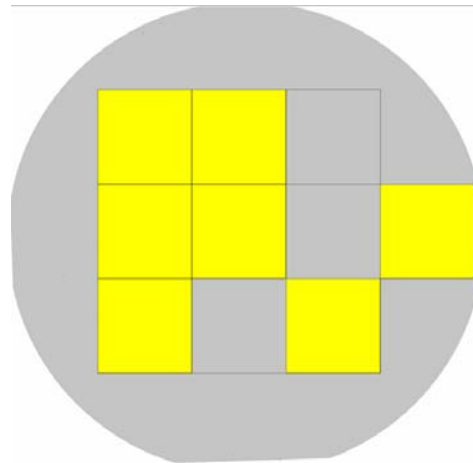


Decreasing Cost of SiC Devices by Scaling Up 150mm Wafers

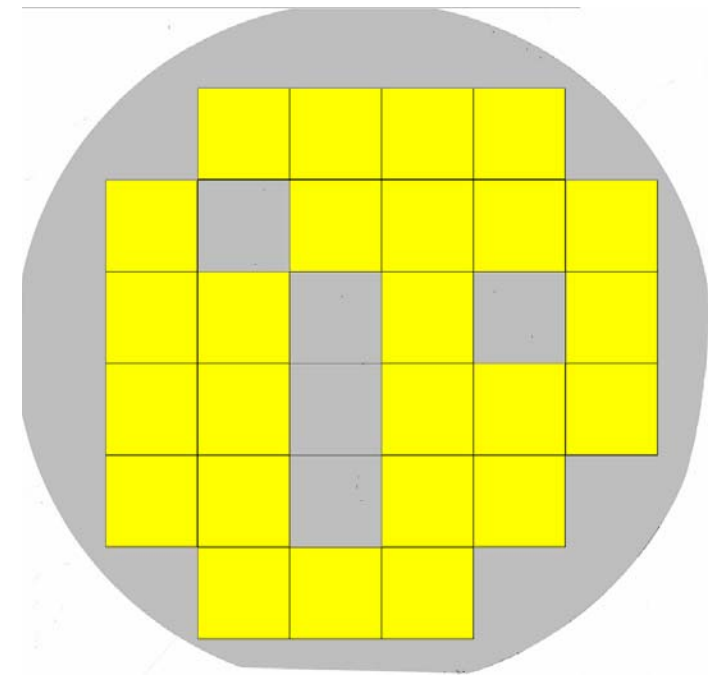
Projected Impact \Rightarrow > 6X More 4 cm² Devices on 150 mm 4HN SiC Wafer



3-inch 4HN-SiC Wafer
 ZMP Wafer MPD = 0 cm⁻²
 4 cm² device yield = 100%
 Yielded 4 cm² devices = 4

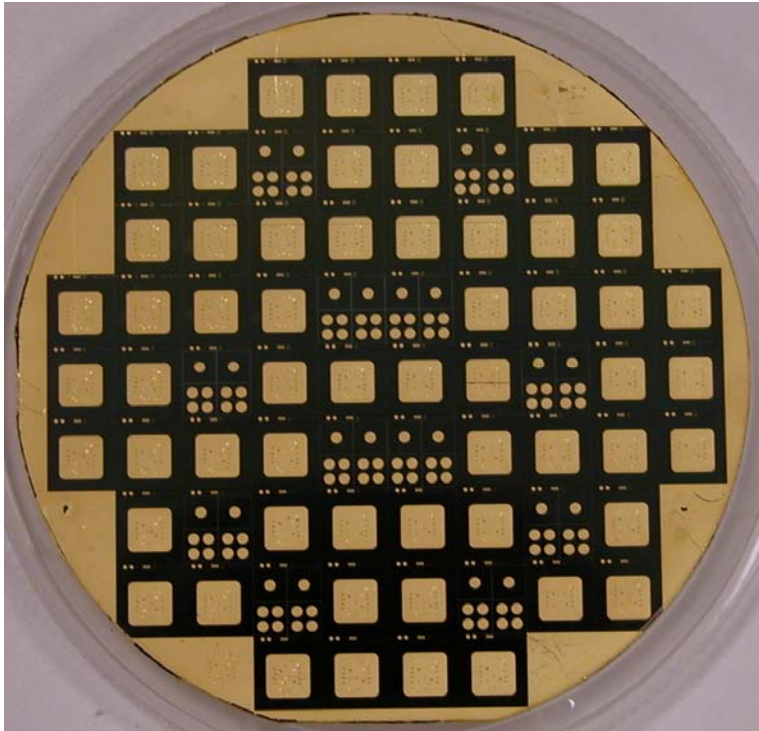


100 mm 4HN-SiC Wafer
 Wafer MPD = 0.20 cm⁻²
 4 cm² device yield = 70%
 Yielding 4 cm² devices = 7

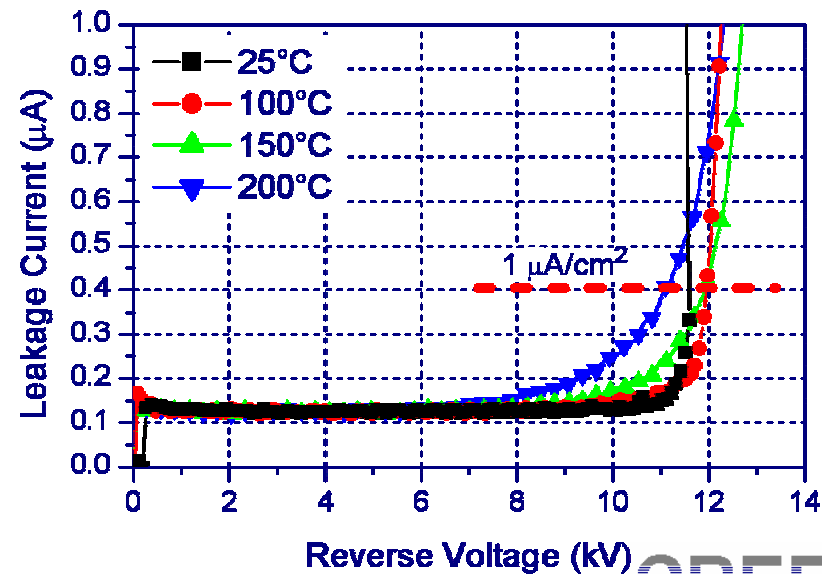
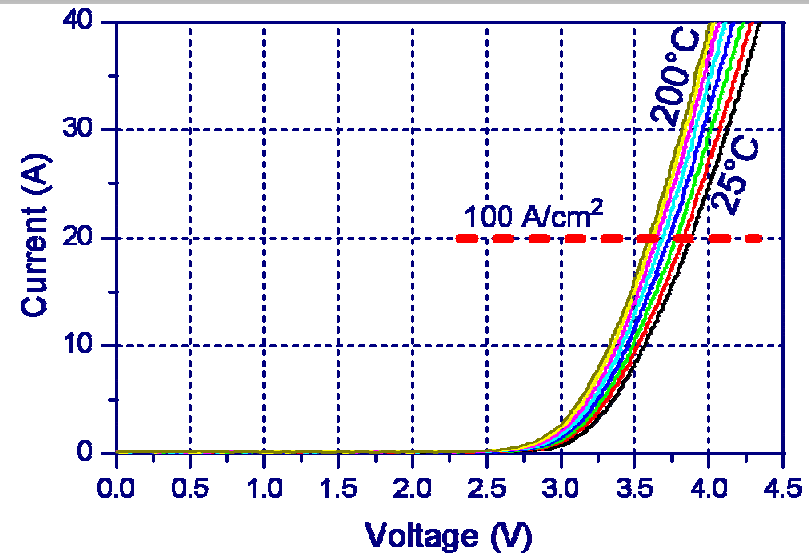


Projected 150 mm 4HN-SiC Wafer
 Estimated MPD = 0.20 cm⁻²
 4 cm² device yield = 83%
 Yielding 4 cm² devices = 25

10kV/20A SiC PiN Diode Characteristics Up to 200°C

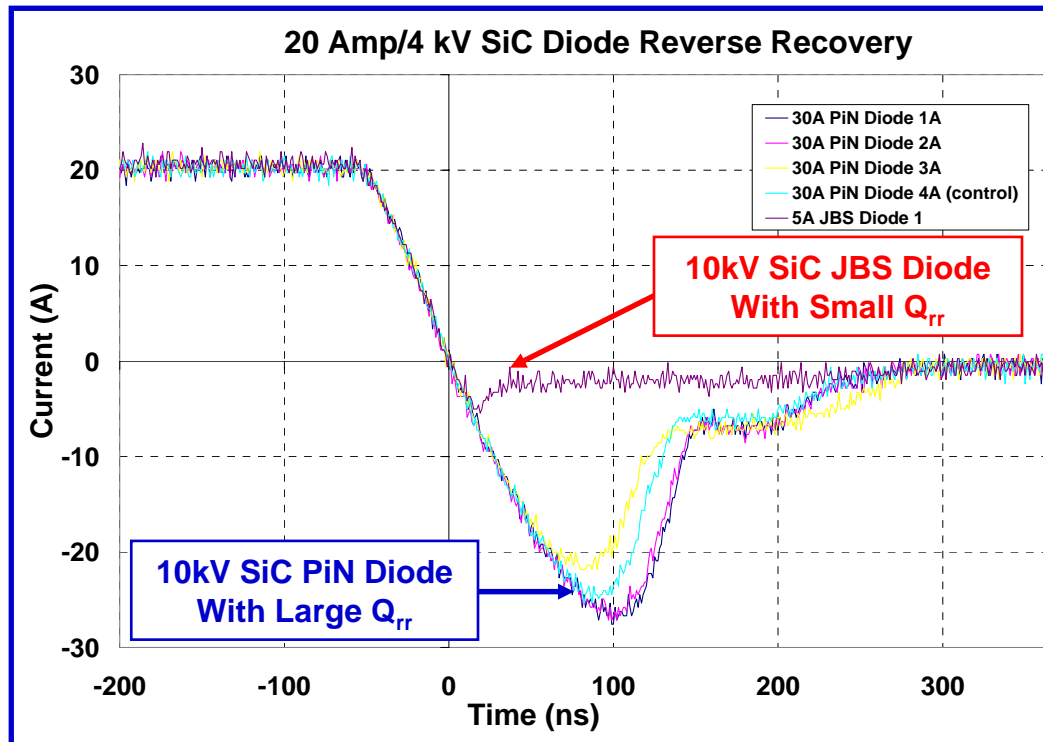


- 10kV/20A SiC PiN Diode
 - $V_F = 3.87$ at 25°C
 - $V_F = 3.60$ at 200°C
 - $V_{BR} > 11.5$ kV
 - $I_R < 300$ nA at 10 kV & $T_j = 200^\circ\text{C}$
- Total SiC PiN Diode Yield ~ 40%





10kV SiC JBS Diode Demonstrated For 20 kHz Switching of SiC Module

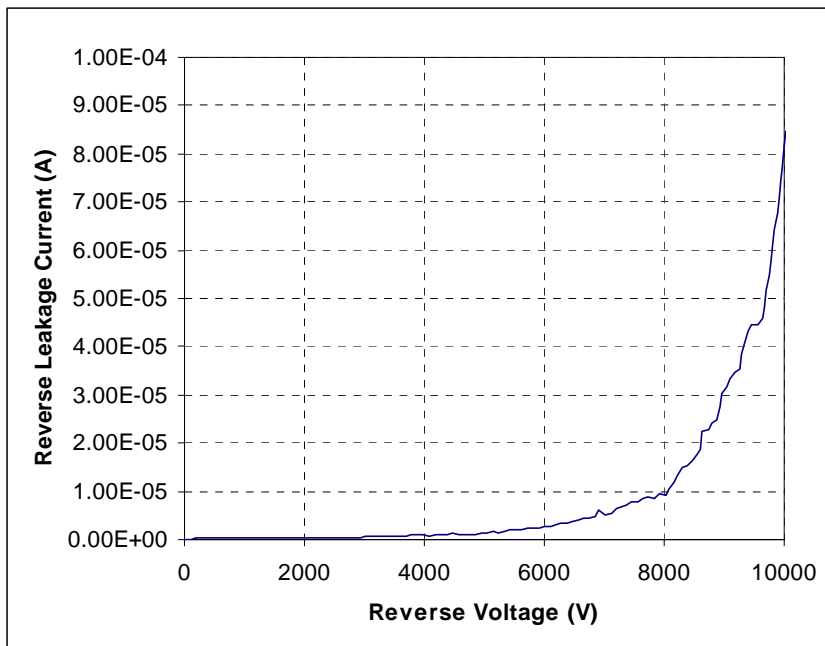


10kV/20A SiC JBS Diode Has Much Smaller Reverse Recovery and Higher Switching Speed Compared to PiN

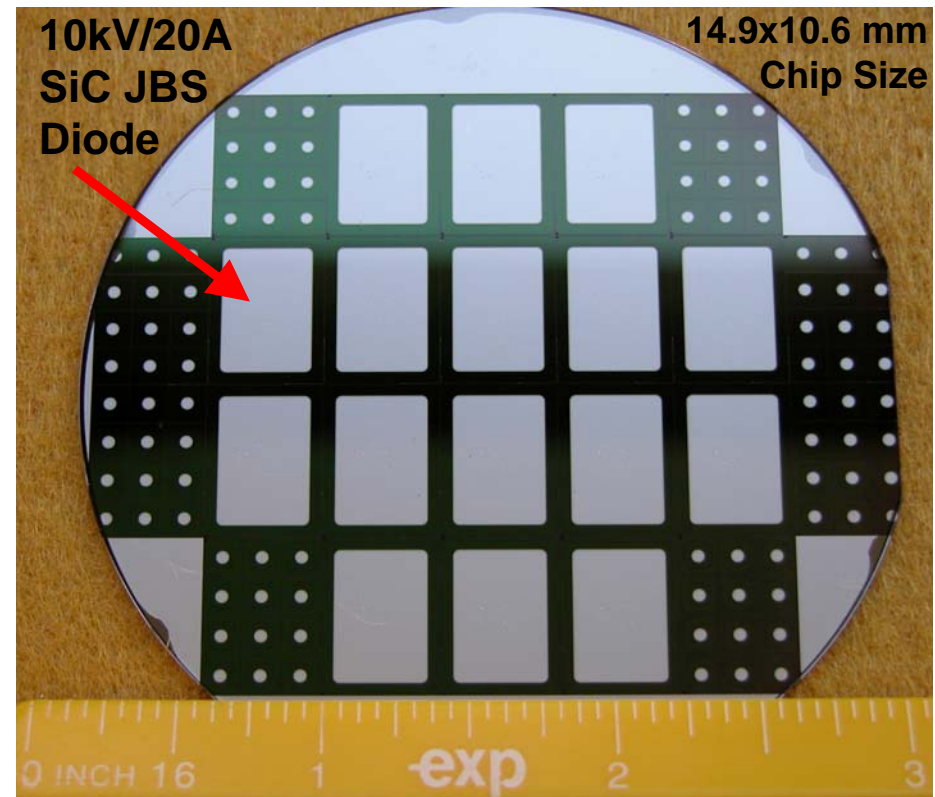
- **SiC PiN Reverse Recovery Energy Dissipation still too high for 20 kHz**
- **Solution - Use SiC Junction Barrier Schottky (JBS) Diodes**
- **Much Smaller Reverse Recovery (Q_{rr}) and Higher Switching Speed**
- **HPE-II Refocused on 10kV/20A SiC JBS Diodes**
- **10kV/5A SiC JBS Diodes Demonstrated with Single Wafer Blocking Yield > 40%**
- **Remaining Issue – 10kV SiC JBS Diode Needs to Be Scaled Up to 20A with 30% Yield**

10kV/20A SiC JBS Diode Device Characteristics

10kV/20A SiC JBS Diode Yield Up to 37%

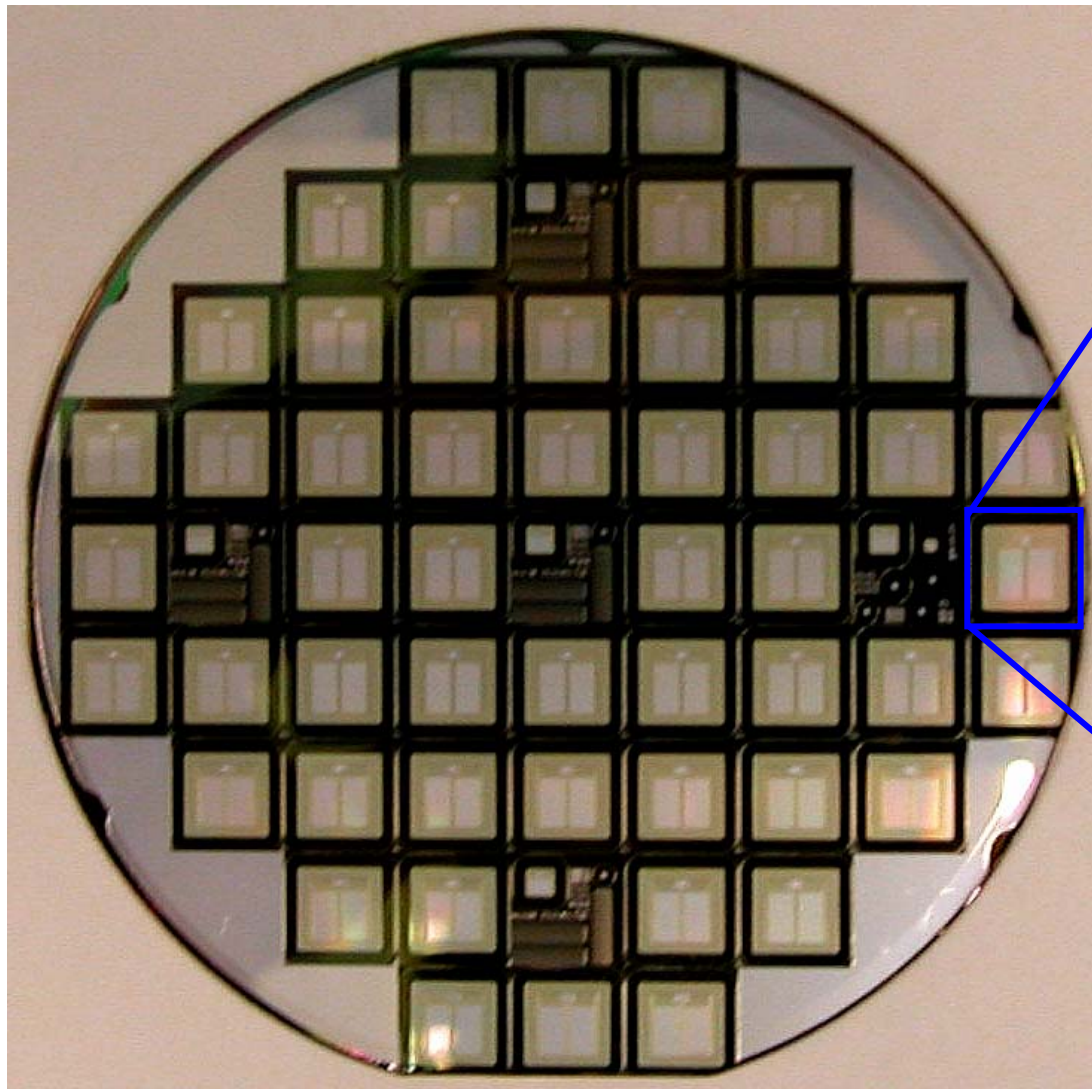


**Reverse Blocking of
10kV/20A SiC JBS Diodes**

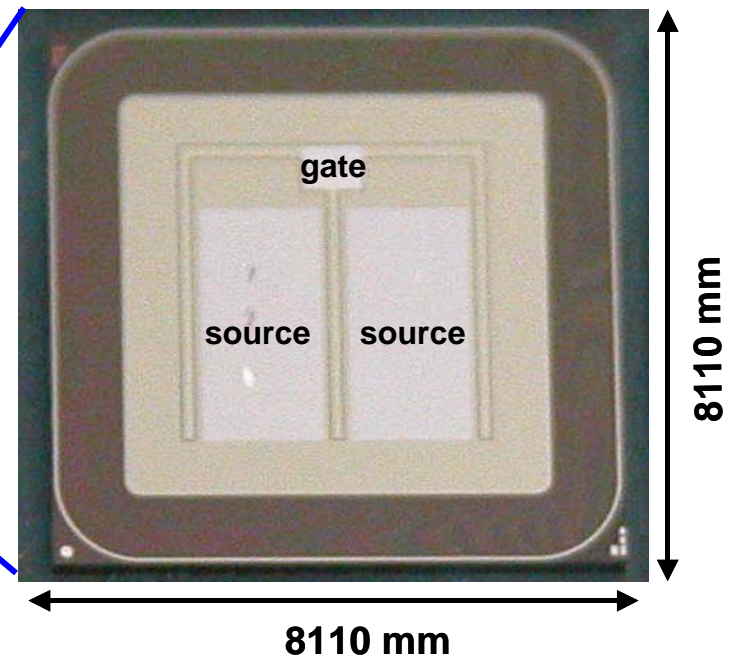


**10kV/20A SiC JBS Diodes
Fabricated on 3-in 4HN-SiC Wafer**

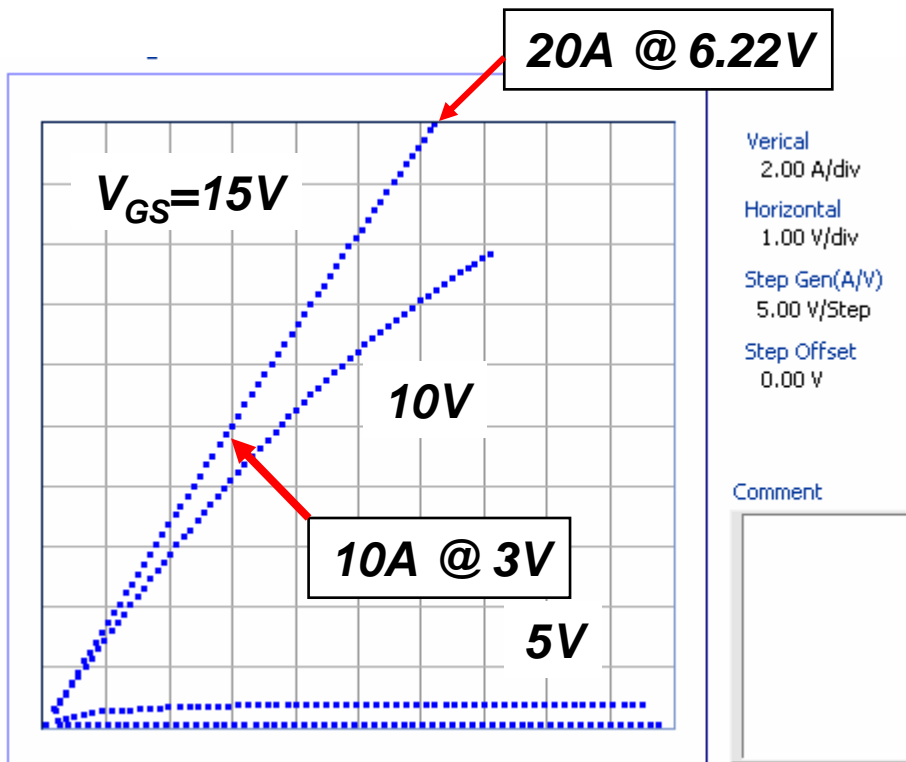
10kV/20A SiC DMOSFET



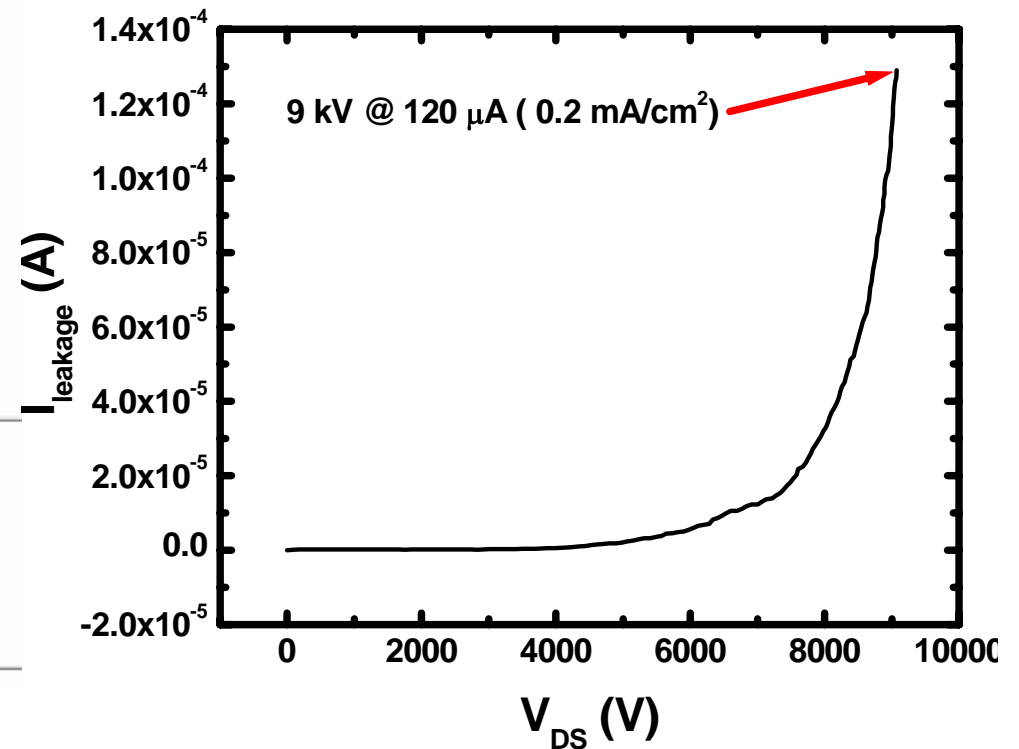
**10kV/20A SiC DMOSFETs
Fabricated on 3-in 4H-SiC Wafer**



9kV/20A SiC DMOSFET Device Characteristics

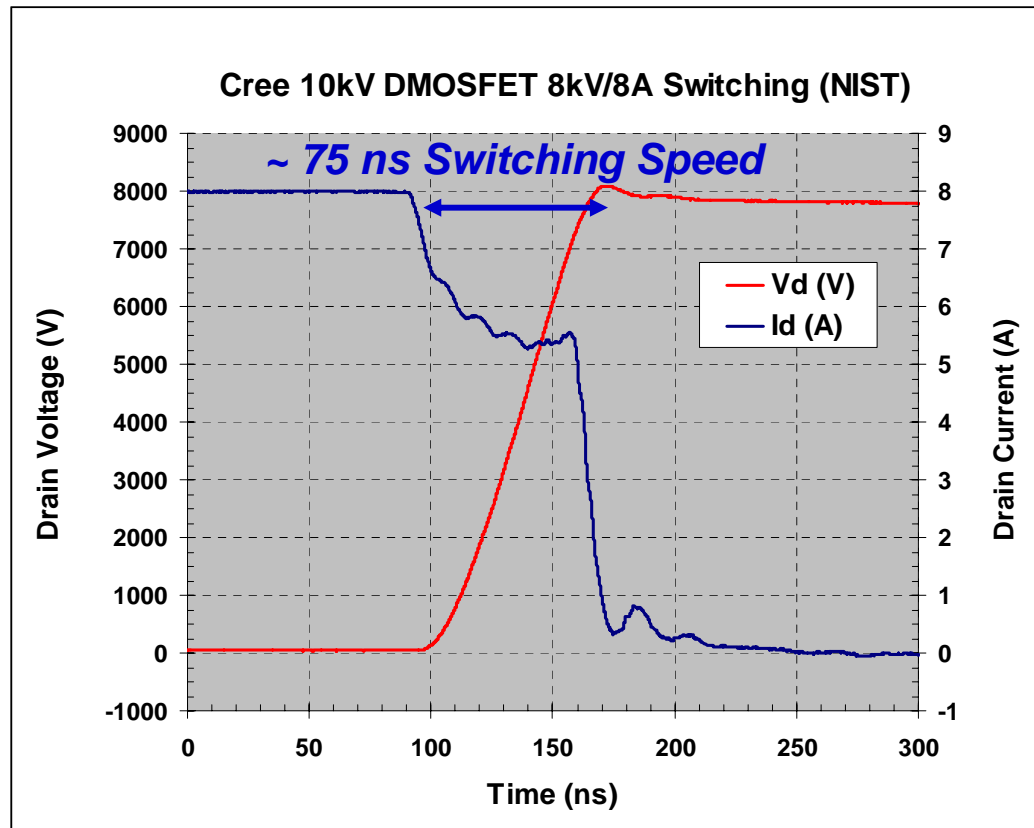


**$R_{on,sp} = 91 \text{ m}\Omega\text{-cm}^2$
20 A @ 189 W/cm²**



$BV > 9 \text{ kV}$

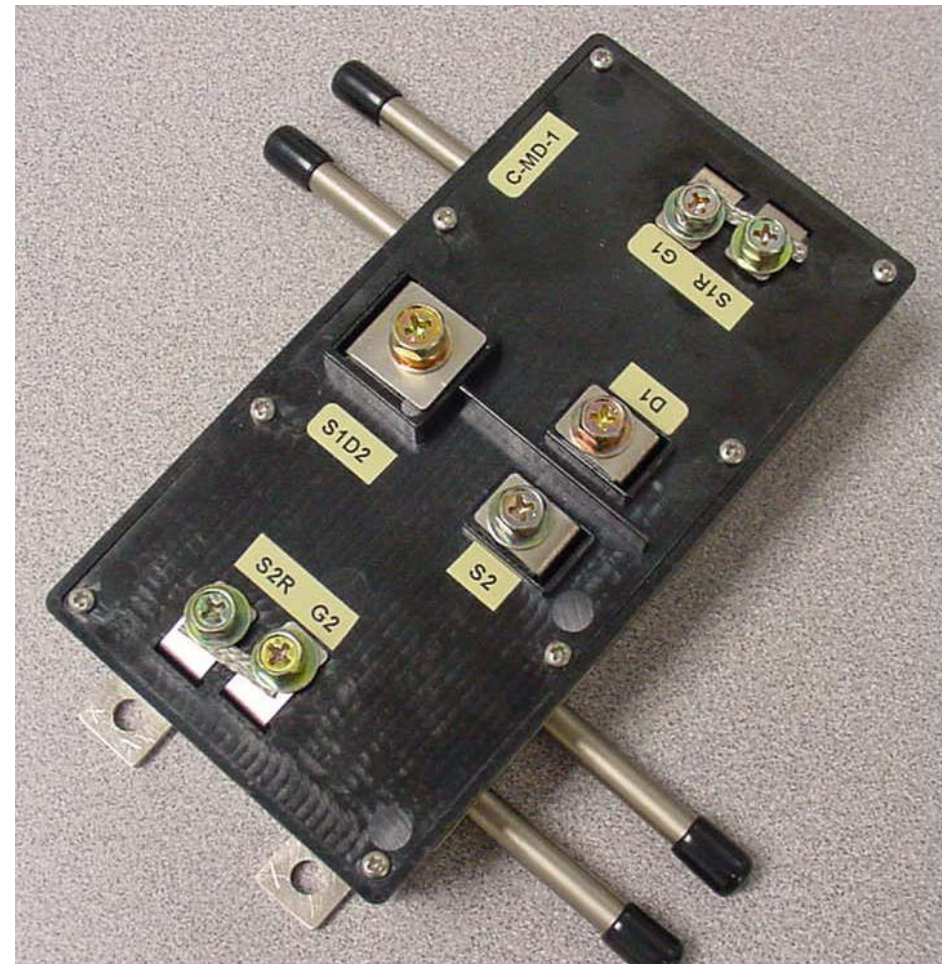
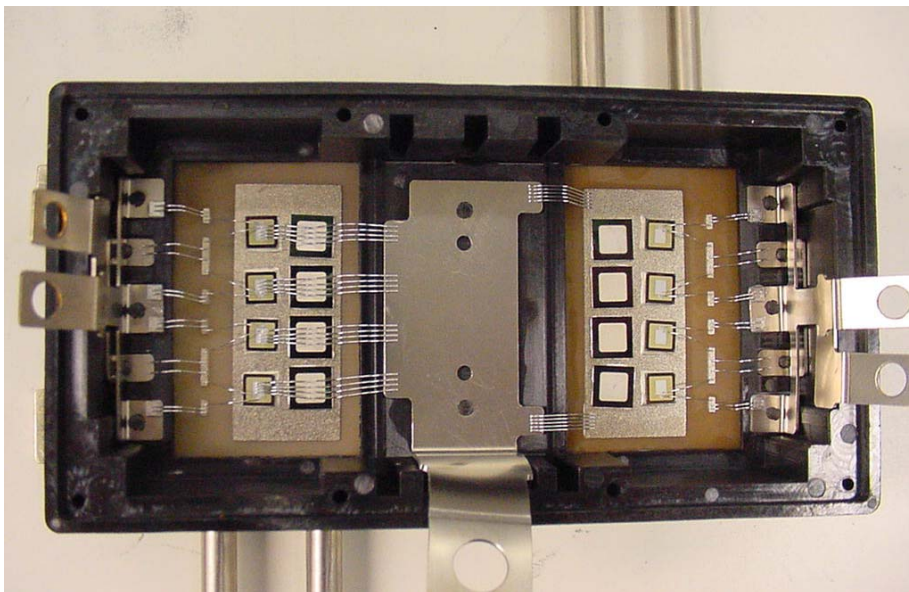
10kV SiC DMOSFET Demonstrated For 20 kHz Switching of SiC Module



- 10kV/10A SiC DMOSFETs Demonstrated
- 10kV SiC DMOSFETs Capable of $T_j = 200^\circ\text{C}$ Operation
- 10kV SiC DMOSFETs Have Switching Speed ~ 75 ns
- Enables 20kHz Switching of 10kV SiC Half H-Bridge Module
- Remaining Issue – 10kV SiC DMOSFET Needs to Be Scaled Up to 20A with 30% Yield

**Measured Switching Speed of ~ 75 ns
for 10kV SiC DMOSFET at 25°C**

10kV/20A SiC DMOSFET Half H-Bridge Module



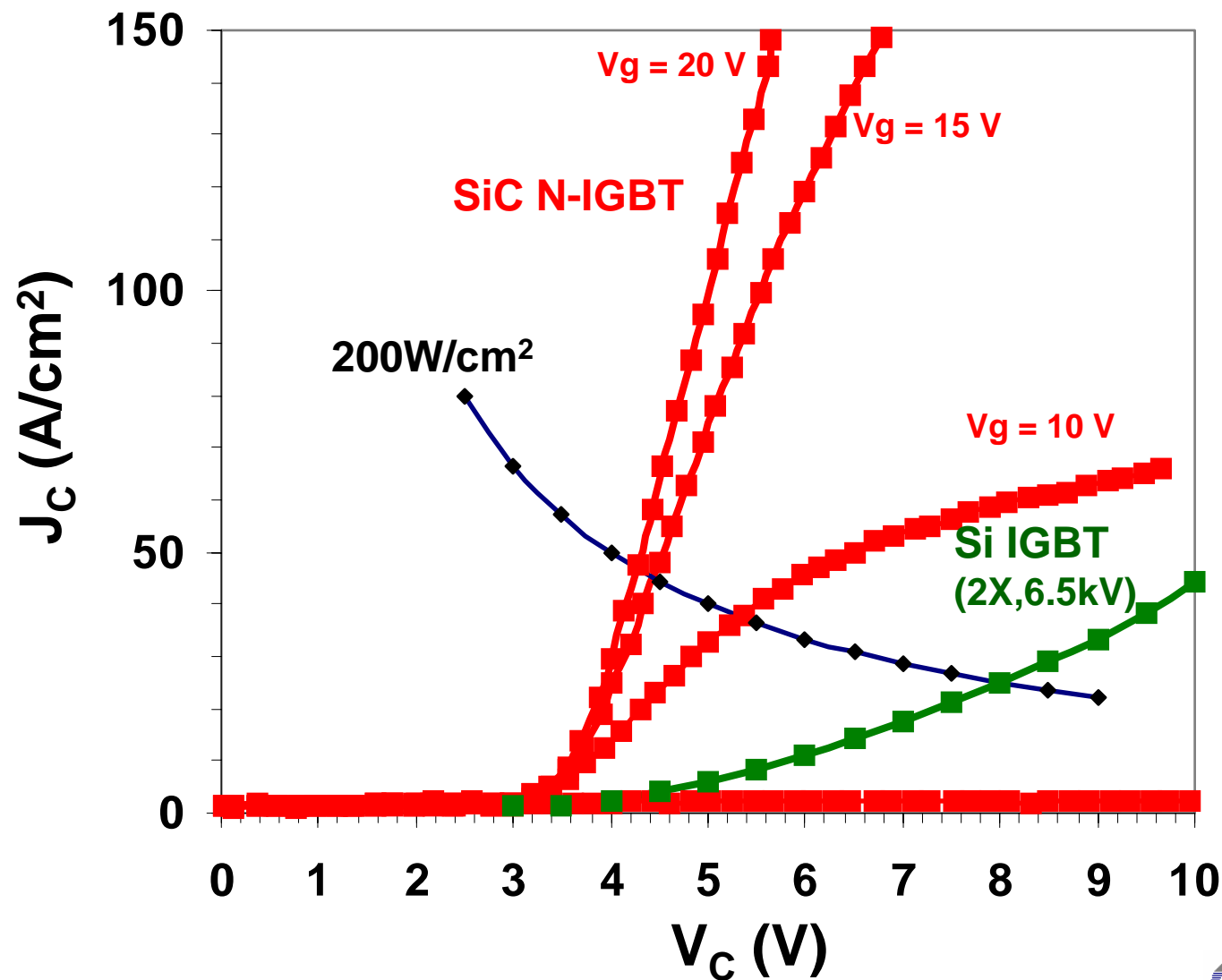


What is next for SiC Power Devices?



- **10 kV pushing upper limit of SiC unipolar devices such as MOSFETs and Schottky diodes**
- **Higher voltage operation will require minority carrier devices (bipolar)**
- **The IGBT is the device used in Si for high speed bipolar switching above 1kV**
- **For SiC, this holds true for >10 kV (10 x the electric breakdown field of silicon)**

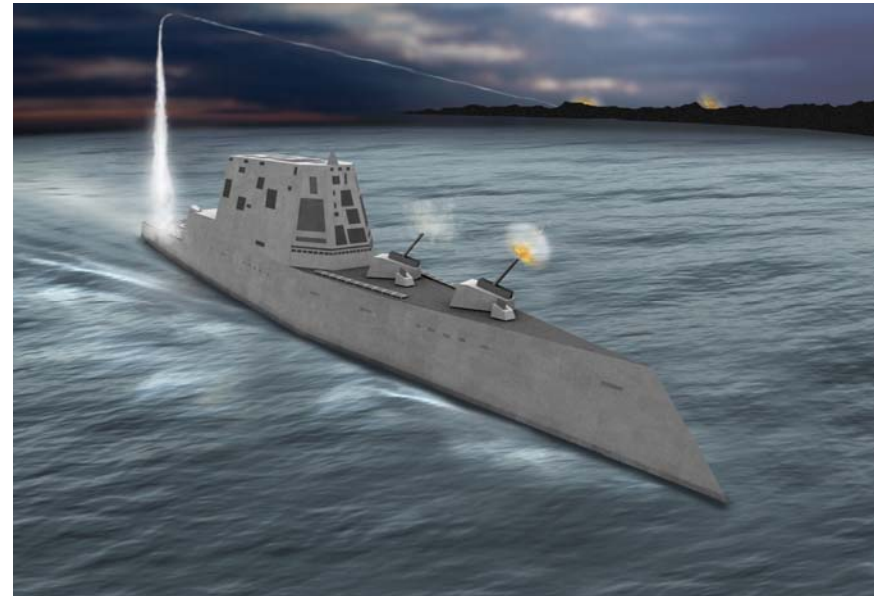
Experimental Results of 12kV SiC N-IGBT and Si IGBT



15 - 20 kV SiC IGBTs Offer Significant Advantages for Future Combat Vessels Using Electrical Power for Propulsion, Aircraft Launch/Recovery & Weapons Systems

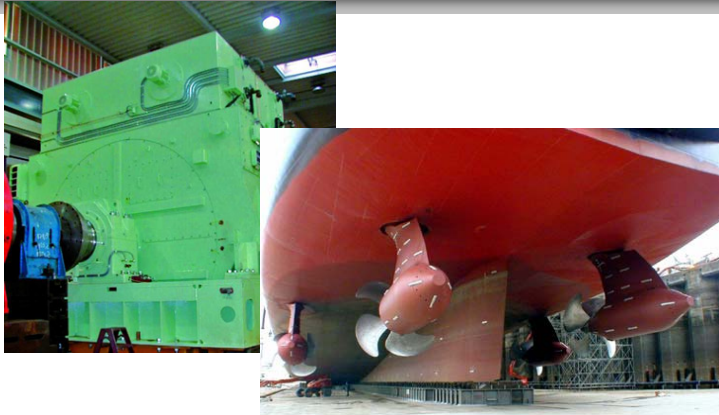


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Navy Applications For SiC IGBTs



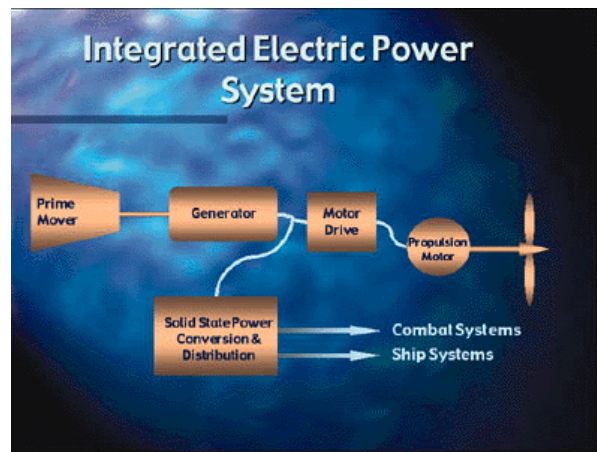
Propulsion

- 4160 V + Motor Drives



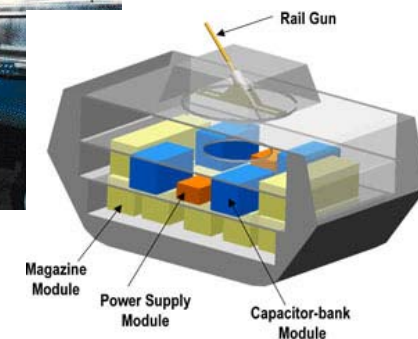
Aircraft Launch and Recovery (EMALS)

- 4 kV Motors



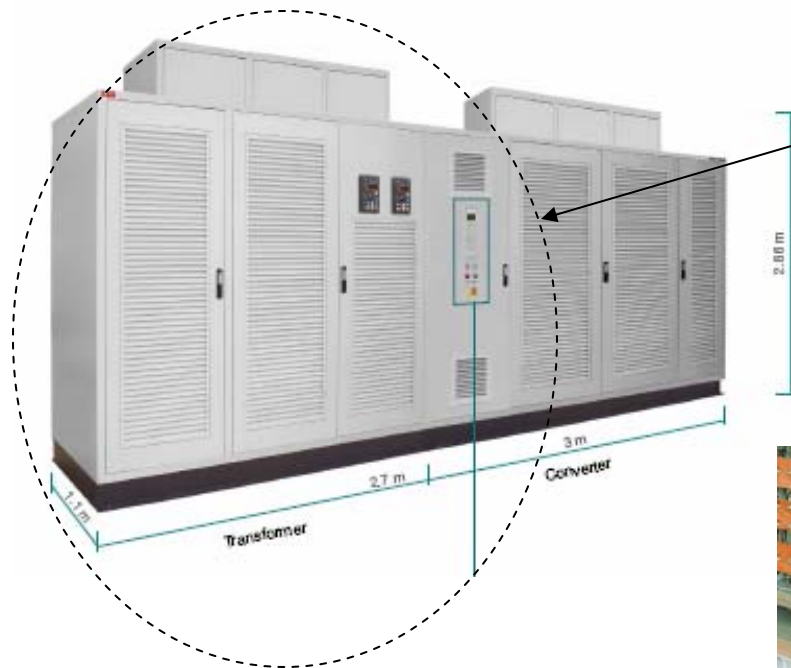
DC Power Distribution

- 6 kV Switchgear



Electromagnetic Gun

Low Voltage Rating of Silicon Switches Addressed Using Complicated Multi-Level Converters

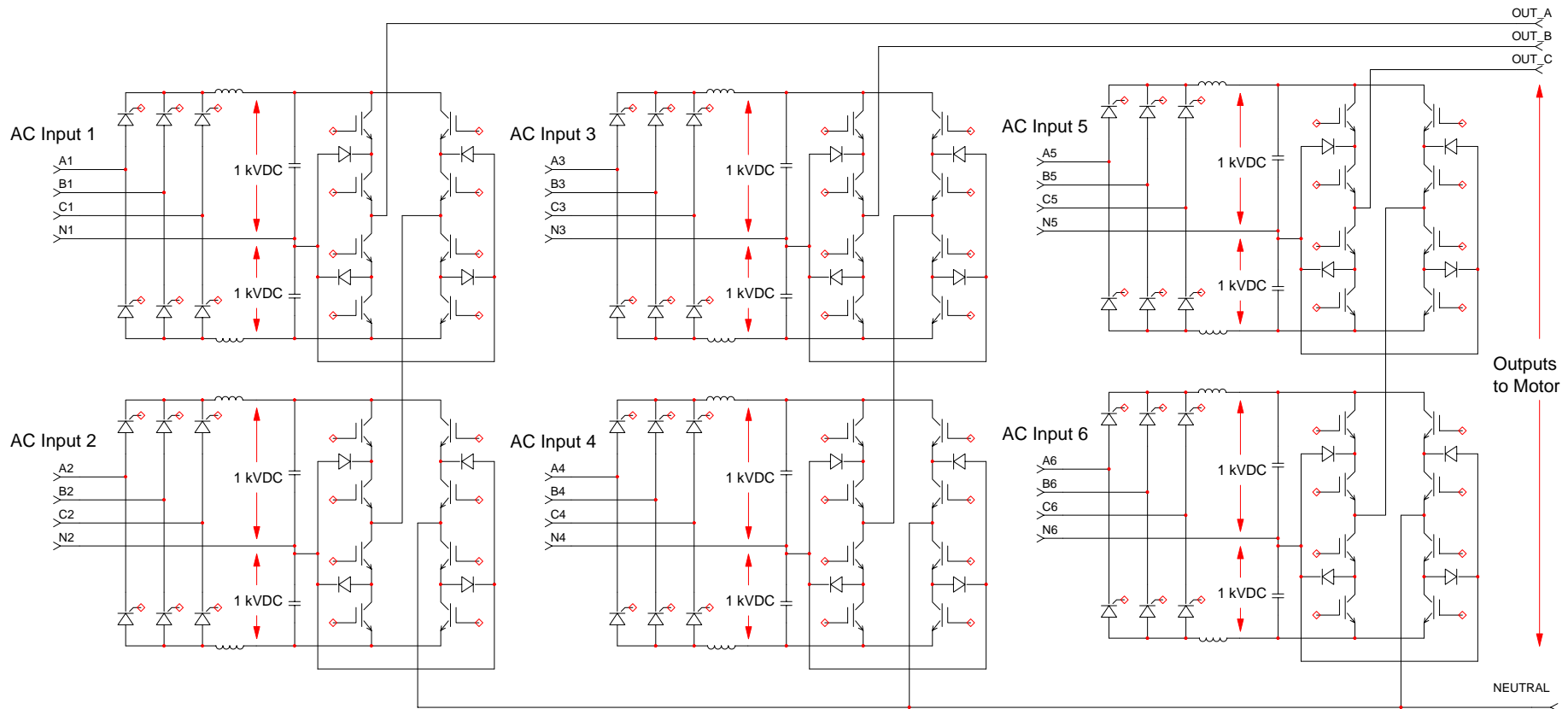


Multi-level converter requires isolated voltages – large line frequency transformer needed that is almost as big as the converter



Several Si switching devices are required

Cascaded Multilevel Converter Suitable for EMALS Based on Si-IGBTs

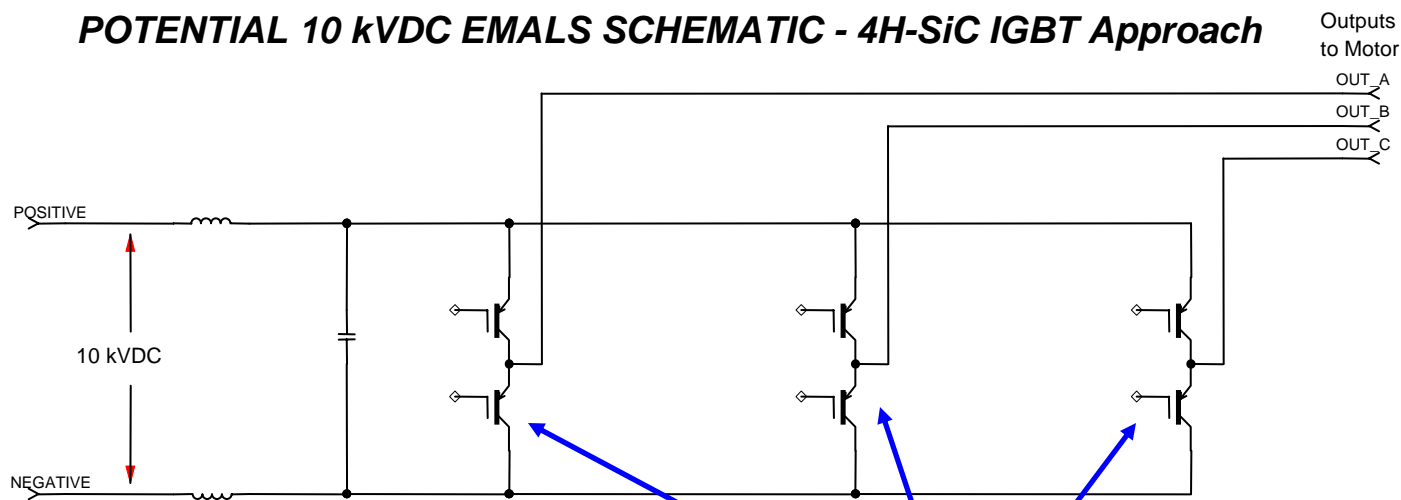


NOTE: ALL IGBTs ASSUMED TO BE REVERSE CONDUCTING

Simplified 2-Level Converter for EMALS Based On 20 kV SiC n-IGBTs

- 20 kV SiC n-IGBTs Used to Implement EMALS Converter Operating from Single Floating 10 kVDC Bus
- Results In Significant Reduction in System Complexity
- Utilize Simple 3-Phase PWM VSI Topology
 - Pulse Width Modulated Voltage Source Inverter Topology

POTENTIAL 10 kVDC EMALS SCHEMATIC - 4H-SiC IGBT Approach



NOTE: ALL IGBTs ASSUMED TO BE REVERSE CONDUCTING

20 kV SiC n-IGBTs



Summary



- **SiC material and device technology has advanced very rapidly under DARPA programs**
- **MOSFETs and Diodes of unprecedented size and voltage demonstrated**
- **150 mm SiC substrates will make large area power devices much more affordable**
- **12 kV SiC IGBTs demonstrated with characteristics far superior to silicon**
- **15-20 kV SiC IGBTs would offer tremendous benefits for electric propulsion, EMALS, and EM Gun applications in form of size, weight, and efficiency**